

Thermodynamic Efficiency Analysis of the S-I Process for Nuclear Hydrogen Production

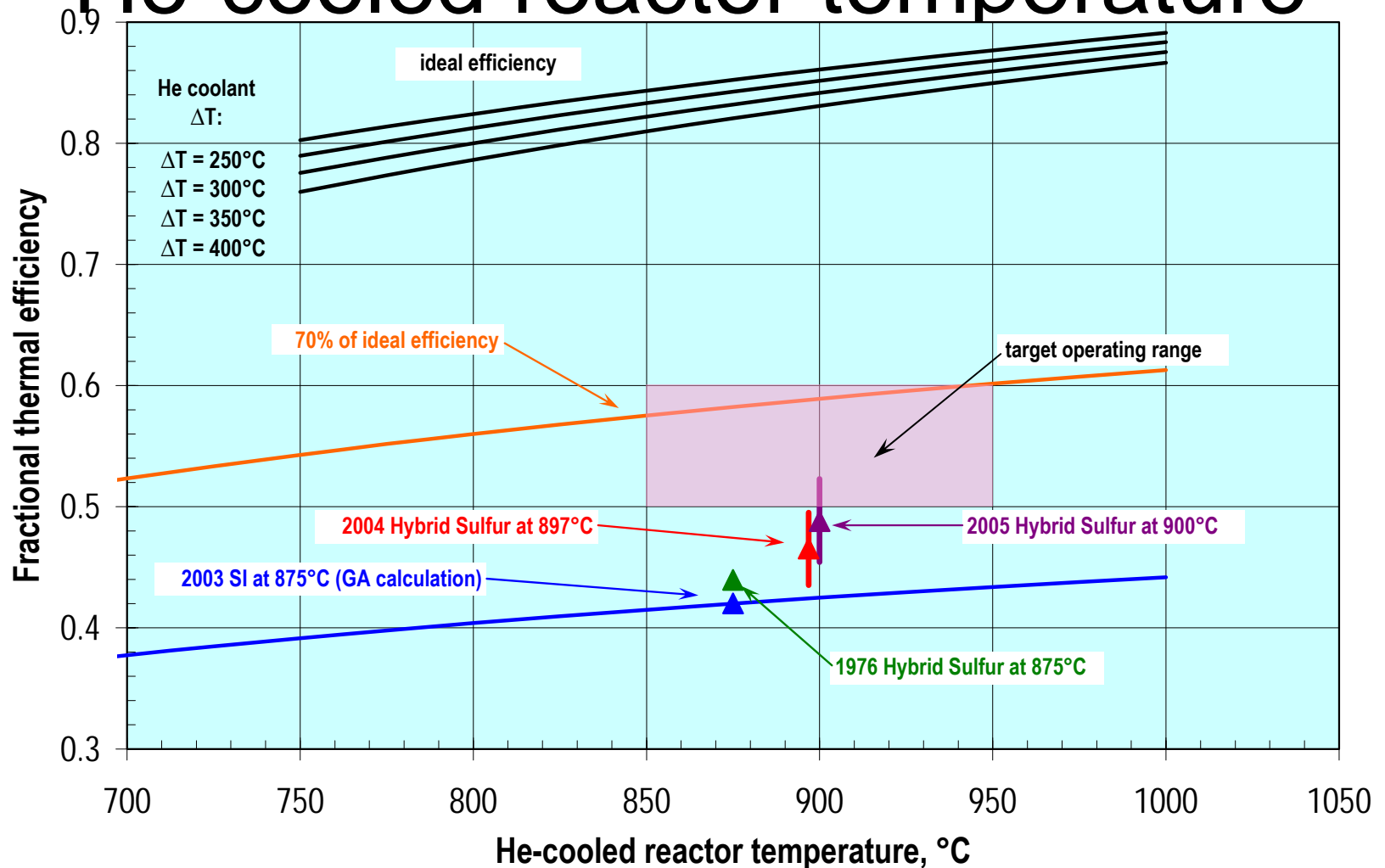
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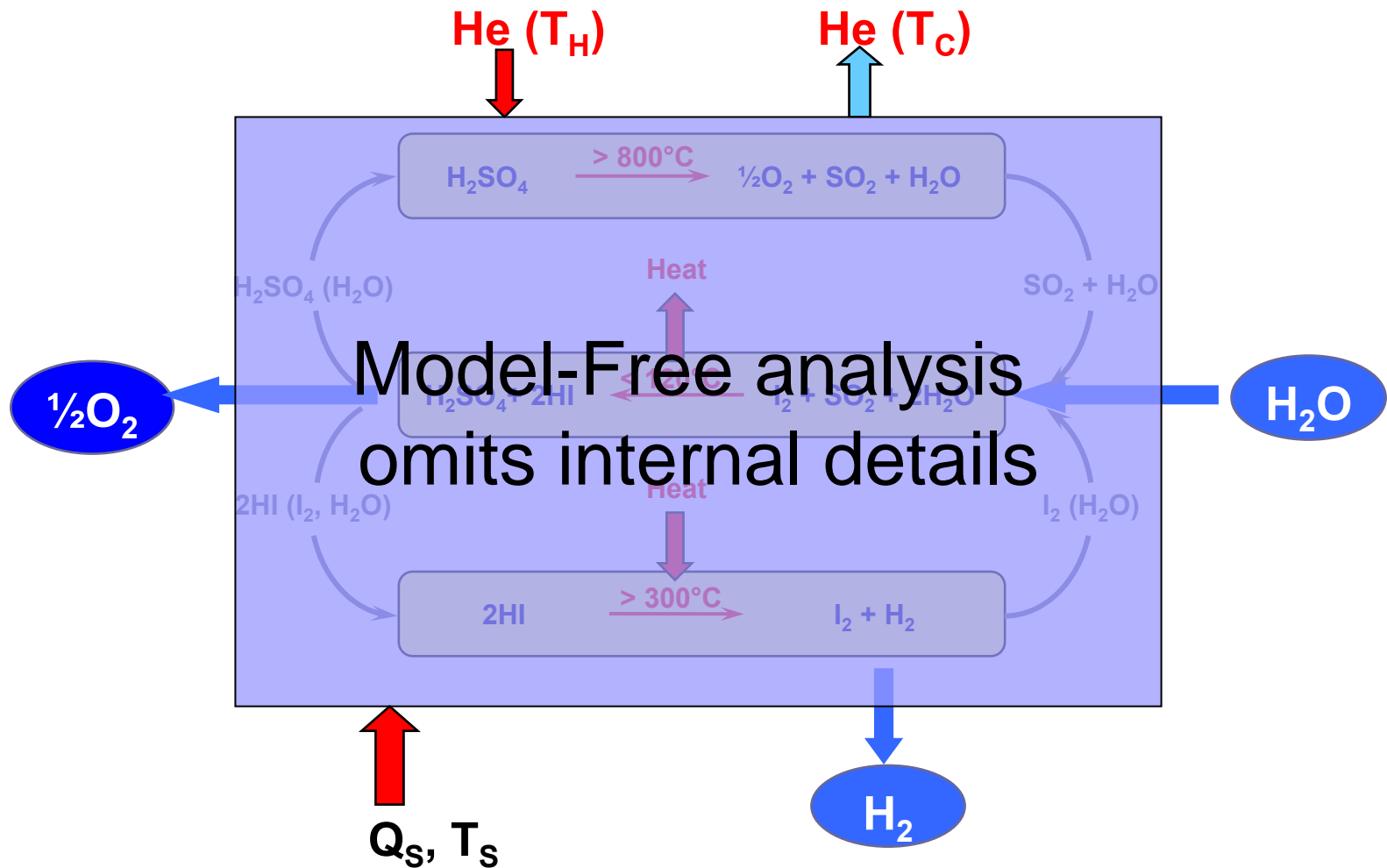
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Thermal efficiency as a function of He-cooled reactor temperature



Sulfur-Iodine (SI) Thermochemical Cycle for H₂ Production



OBJECTIVES

- Set up procedure for, & obtain, reversible process limits for idealized & simulated Sulfur-Iodine H₂ generation sections
- Minimize influence of model properties & process units – “model-free”
- Use as basis to compare effects on efficiency of configurations & flows
- Determine sensitivities to guide data taking for reliable simulations
- Perhaps suggest novel process concepts

GENERAL APPROACH

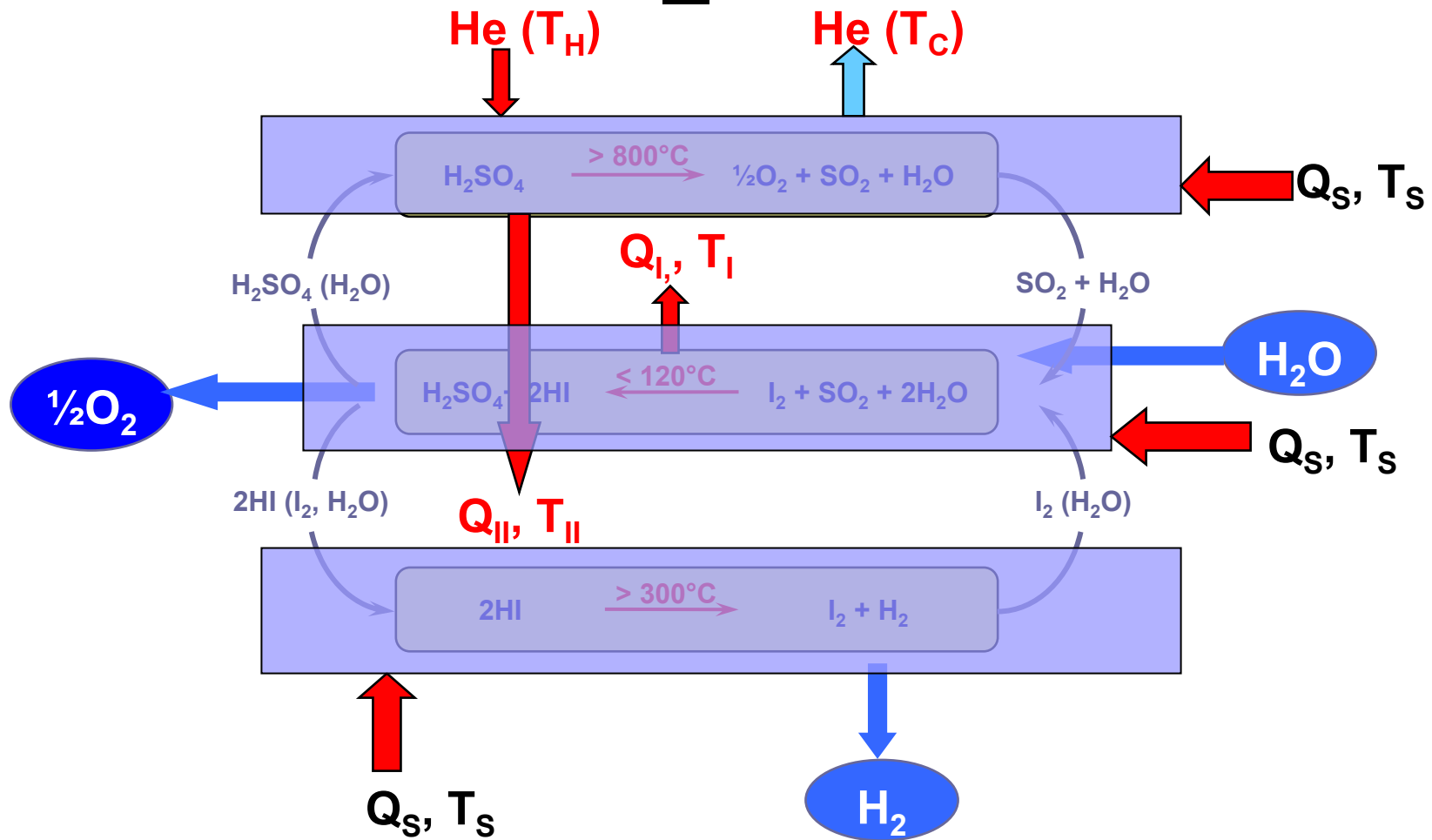
- Use steady-state 1st & 2nd Law equations for reversible/reversible systems with material & energy flows on sections & overall process
- 1st Law

$$\sum_{\text{inlet ports}} \dot{m}h_i - \sum_{\text{outlet ports}} \dot{m}h_o + \sum_{\text{heats}} \dot{Q}_H + \sum_{\text{machines}} \dot{W} = 0$$

- 2nd Law (reversible for $\dot{S}_{gen} = 0$)

$$\sum_{\text{inlet ports}} \dot{m}s_i - \sum_{\text{outlet ports}} \dot{m}s_o + \sum_{\text{heats}} \frac{\dot{Q}_H}{T_H} + \dot{S}_{gen} = 0$$

Sulfur-Iodine (SI) Thermochemical Cycle for H₂ Production

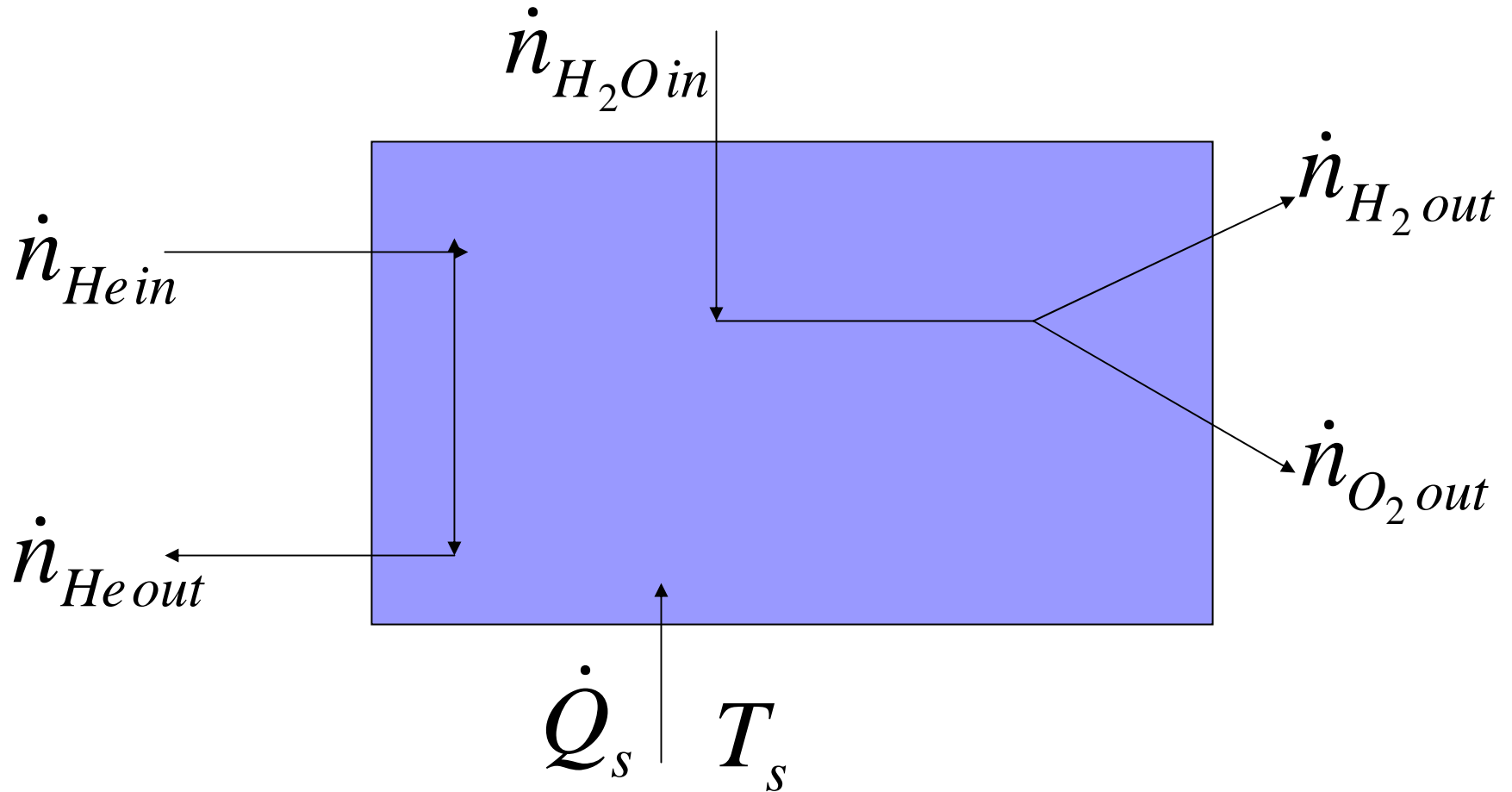


Use Analysis to Determine Q_i, Q_S of Sections

SOLVE FOR 2 VARIABLES

- Variables:
 - Inlet/outlet streams: $T, P, \dot{n}_i, \dot{n}_o$
 - Heat effects: \dot{Q}_I & \dot{Q}_S
- Use property model relations for reaction & stream enthalpies, h , entropies, s
- Use 2 equations to solve for 2 variables of:
 - Overall water-splitting system
 - S-I sections I-III with only reactant/products
 - S-I sections I-III with recycled components
- For reversible compared to real, 1 condition different
- For irreversible what S_{gen} matches real conditions?

OVERALL WATER SPLITTING



$$\dot{n}_{Heout} = \dot{n}_{Hein} \quad \dot{n}_{H_2out} = 2\dot{n}_{O_2out} = \dot{n}_{H_2Oin} = 1 \text{ kmol/hr}$$

WATER SPLITTING BALANCES

$$\dot{n}_{He\ in} (h_{He\ in} - h_{He\ out}) - \dot{n}_{H_2\ out} (h_{H_2\ out} + \frac{1}{2} h_{O_2\ out} - h_{H_2O\ in}) + \dot{Q}_s = 0$$

$$\dot{n}_{He\ in} c_{p,He} (T_{He\ in} - T_{He\ out}) - \dot{n}_{H_2\ out} \Delta H_{WS} + \dot{Q}_s = 0$$

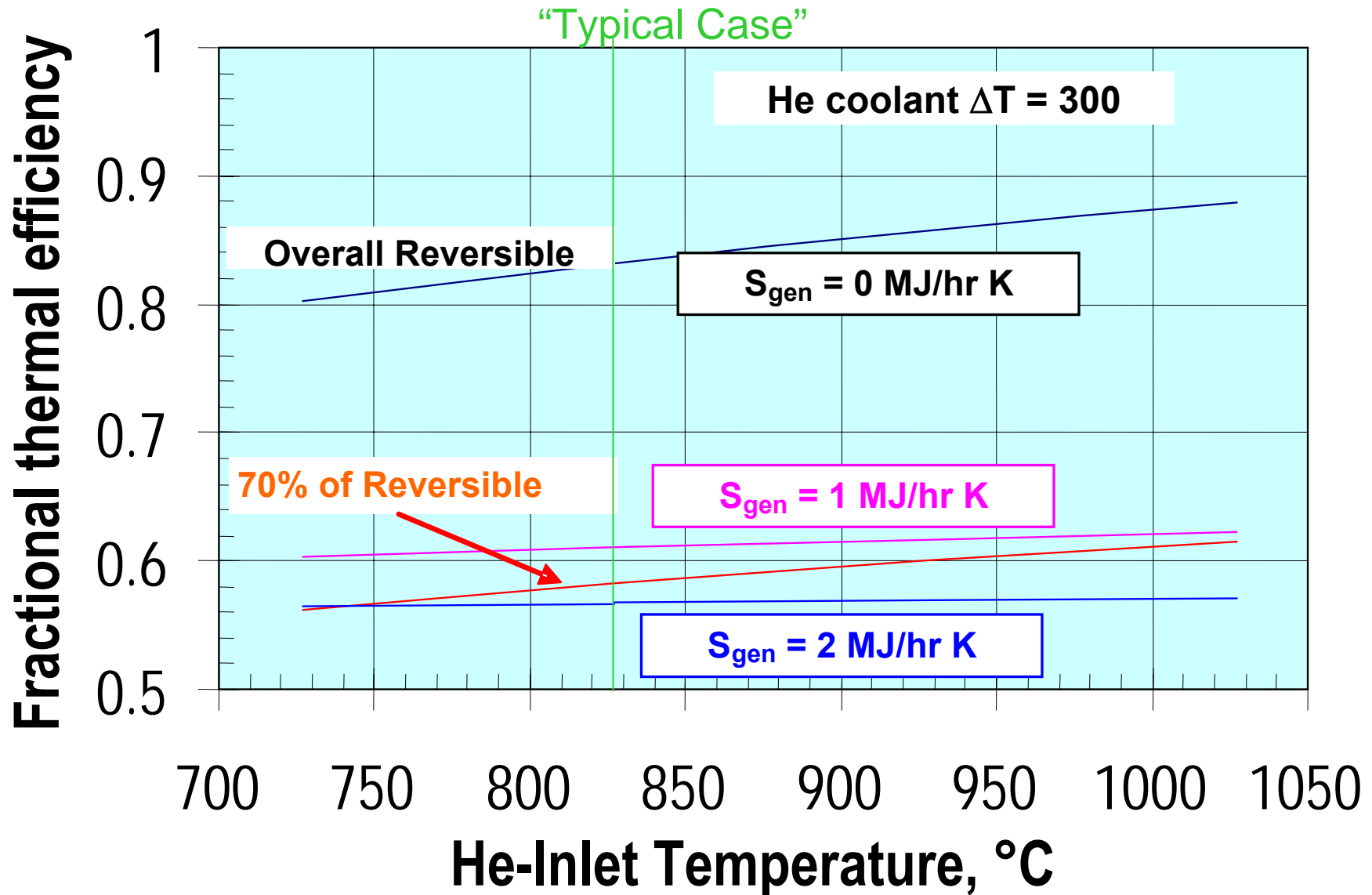
$$\dot{n}_{He\ in} (s_{He\ in} - s_{He\ out}) - \dot{n}_{H_2\ out} (s_{H_2\ out} + \frac{1}{2} s_{O_2\ out} - s_{H_2O\ in}) + \frac{\dot{Q}_s}{T_s} + S_{gen} = 0$$

$$\dot{n}_{He\ in} \left[c_{p,He} \ln \left(\frac{T_{He\ in}}{T_{He\ out}} \right) - R \ln \left(\frac{P_{He\ in}}{P_{He\ out}} \right) \right] - \dot{n}_{H_2\ out} \Delta S_{WS} + \frac{\dot{Q}_s}{T_s} + S_{gen} = 0$$

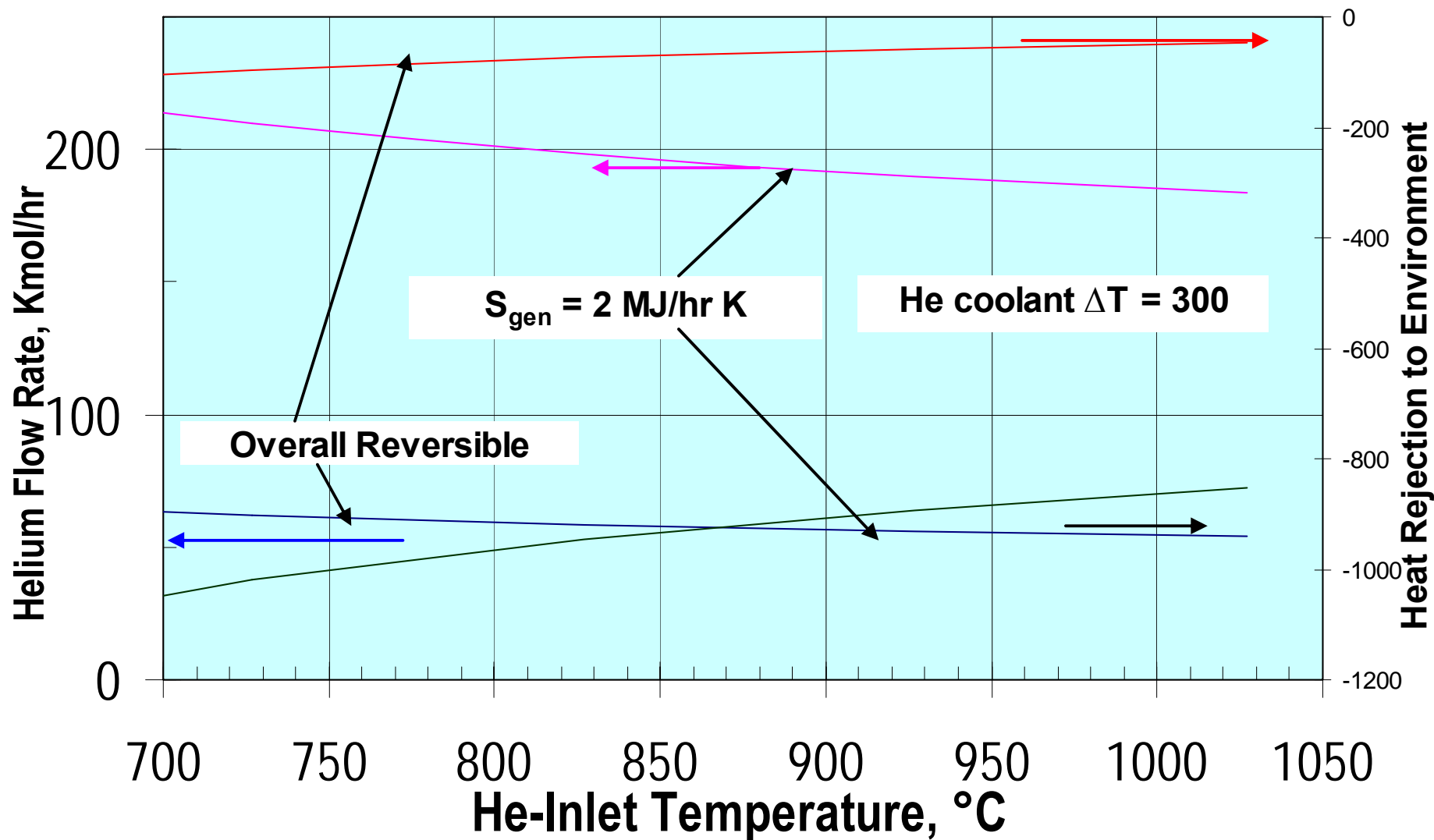
Choose $T_{He\ out}$, $P_{He\ out}$, $P_{He\ in}$, T_s ; range of $T_{He\ in}$

Set $c_{p,He}$, ΔH_{WS} , ΔS_{WS} , S_{gen} Solve for \dot{Q}_s & $\dot{n}_{He\ in} \Rightarrow \eta$

OVERALL WATER SPLITTING



He & Heat Flows for Water-Splitting



EQUATIONS FOR SECTIONS

Reversible

■ 1st Law

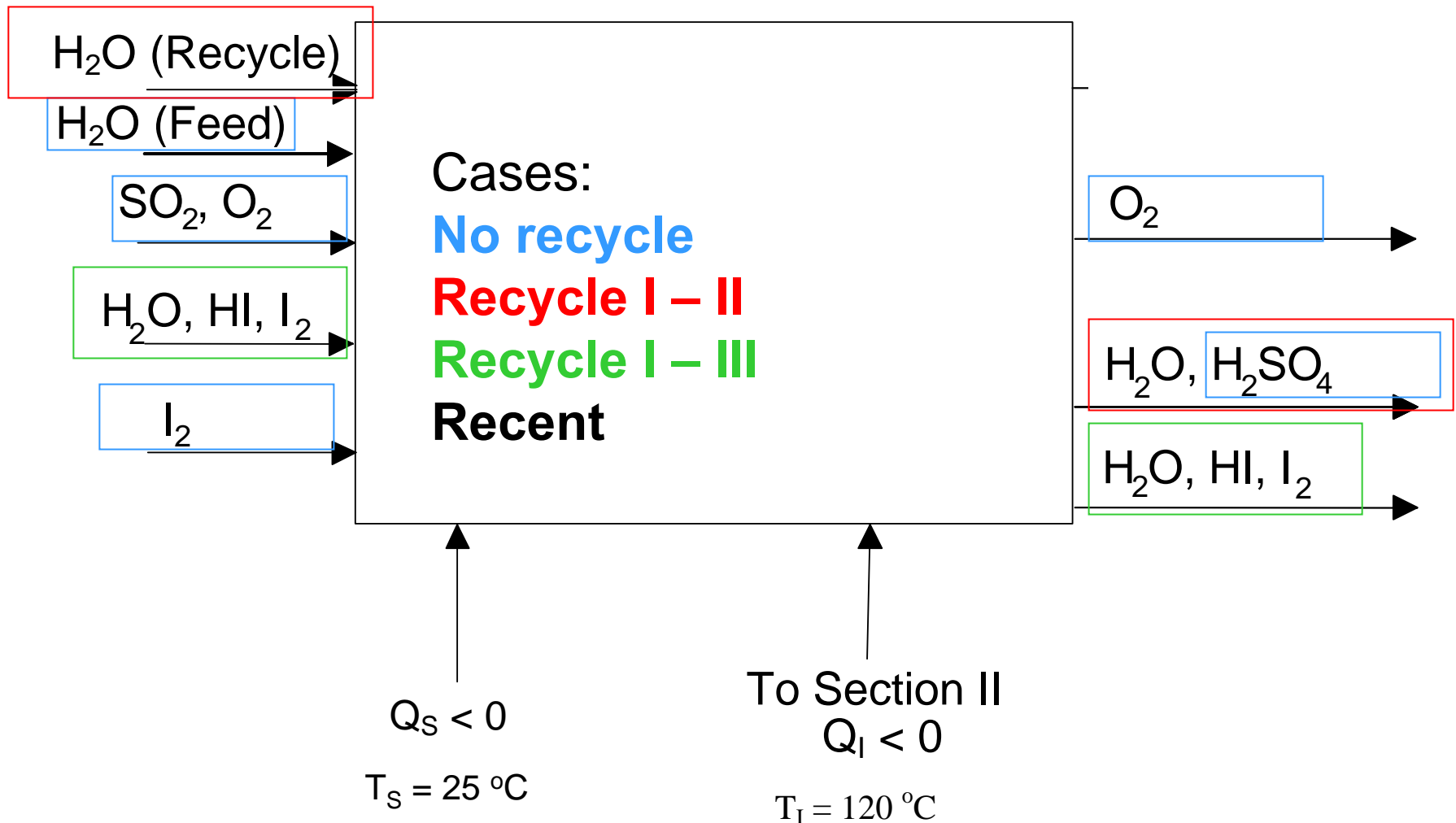
$$\sum_{\text{inlet ports}} \dot{m}h_i - \sum_{\text{outlet ports}} \dot{m}h_o + \dot{Q}_I + \dot{Q}_S = 0$$

■ 2nd Law (reversible for $\dot{S}_{gen} = 0$)

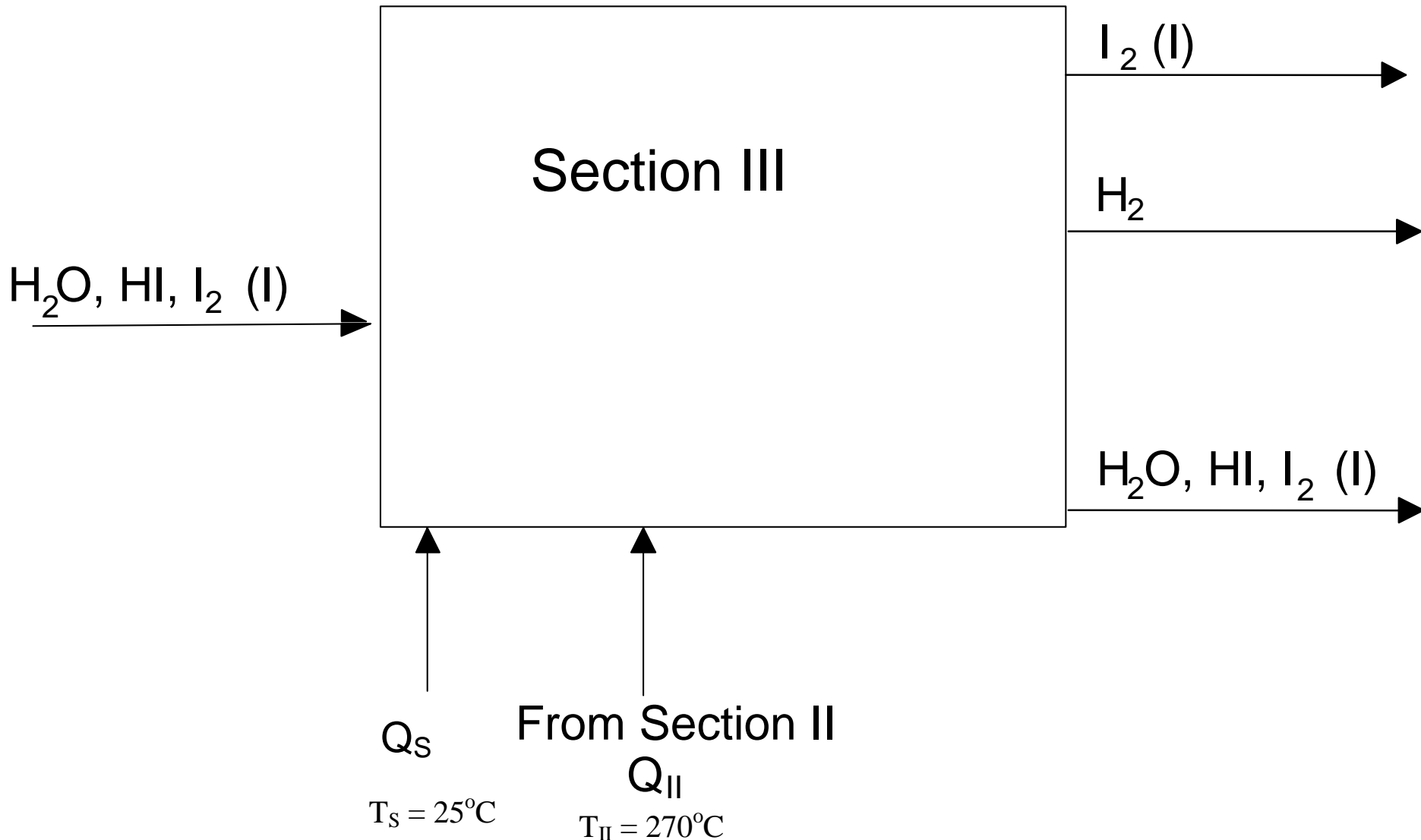
Irreversible

$$\sum_{\text{inlet ports}} \dot{m}s_i - \sum_{\text{outlet ports}} \dot{m}s_o + \frac{\dot{Q}_I}{T_I} + \frac{\dot{Q}_S}{T_S} + \dot{S}_{gen} = 0$$

MATERIAL FLOWS SECTION I



MATERIAL FLOWS SECTION III



TYPICAL SECTION RESULTS

Case	Q_I to II MJ/hr	Q_{II} to III MJ/hr	Q_S MJ/hr	He Flow Kmol/hr
Reversible ($S_{gen} = 0$)				$T_{He In} = 827^\circ\text{C}; T_{He Out} = 527^\circ\text{C}$

CONCLUSIONS

- Model-free analysis shows
 - Overall process can have high efficiency
 - For reversible sections, adding recycles leads to large internal heat flows, unchanged He flow & heat rejection
 - For irreversible sections, internal heat flows further increased, He flow & heat rejection much greater
 - Section I-II recycle has less effect than I-III
- Further study to uncover sensitivities, specific locations for efficiency focus